

Status of SC-DD FE Electronics for MIPs Timing

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for

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of
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Measurements

Focus on noise and rise time!

About setup

PULSE GENERATOR: 9210+9214/LeCroy

- $U_{\text{GEN}} = \pm(500 \rightarrow 5000\text{mV})$
- $T_{\text{W}} = 1\text{ns} \rightarrow 100\text{ms}$
- edge= 300ps, fixed
- $F_{\text{REP}} = \text{max. } 300\text{MHz}$

ATTENUATOR: Suhner

- atten=10, 20 db
- impedance=50 Ω
- B=4GHz

OSCILLOSCOPE: WavePro 7300/ LeCroy

- B=3GHz
- Sampling rate= max. 20GS/s

DUT

2 charge sens amps:

- CSPA – M. Ciobanu version
 - FCSA – Al. Martemyanov version
- 2 broadband amps:
- DBA2 – P. Moritz
 - BB4 – W. König

Measurements

About settings

TEST PULSE

Selected

- T_P and T_N transitions
- minimum amplitude (500mV)

To have

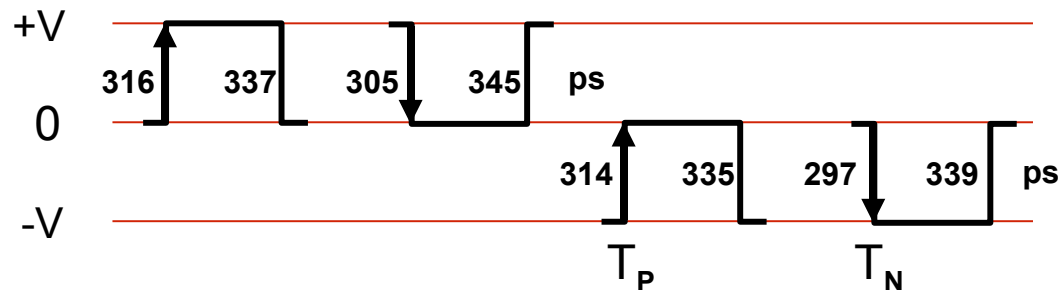
- fastest transition
- best shape

ATTENUATOR

Selected

- minimum number of attenuators

Pulse generator can deliver:



Attenuator contribution to rise time (estimated)

No. of atten.	1	2	3	
B	4	2.8	2.3	GHz
T_R	88	124	152	ps
Influence on 300ps rise time	313	325	336	ps

Measurements

About settings

AMPLITUDE SCALE

- Rise time measurements →

2nd atten. effect

lower bandwidth effect

Selected ≥10mV/div

U_{GEN}	500					mV
Atten.	0	10	20	10+20	10+20	db
U_{IN}	500	160	50	16	16	mV
T_N	297	301	299	305	338	ps
T_P	314	316	315	324	355	ps
Amplit. scale	100	50	10	10	5	$\frac{mV}{div}$

- Noise measurements →

lower bandwidth effect

Selected ≥10mV/div, $N_{pkpk} \sim 1div$

Noise	1.62	1.65	1.70	1.55	1.00	mV_{RMS}
Amplit. scale	50	20	10	5	2	$\frac{mV}{div}$

TIME SCALE

- Rise time measurements →

Selected 2ns/div (better estimated pulse amplitude)

T_R	305	304	304		ps
Time scale	0.5	1	2		$\frac{ns}{div}$

- Noise measurements

Selected 50ns/div

TRIGGER LEVEL

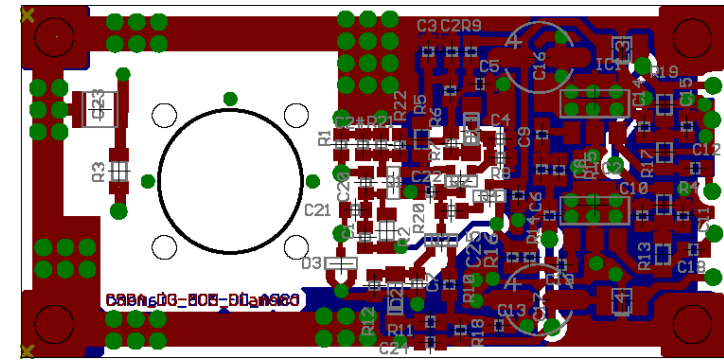
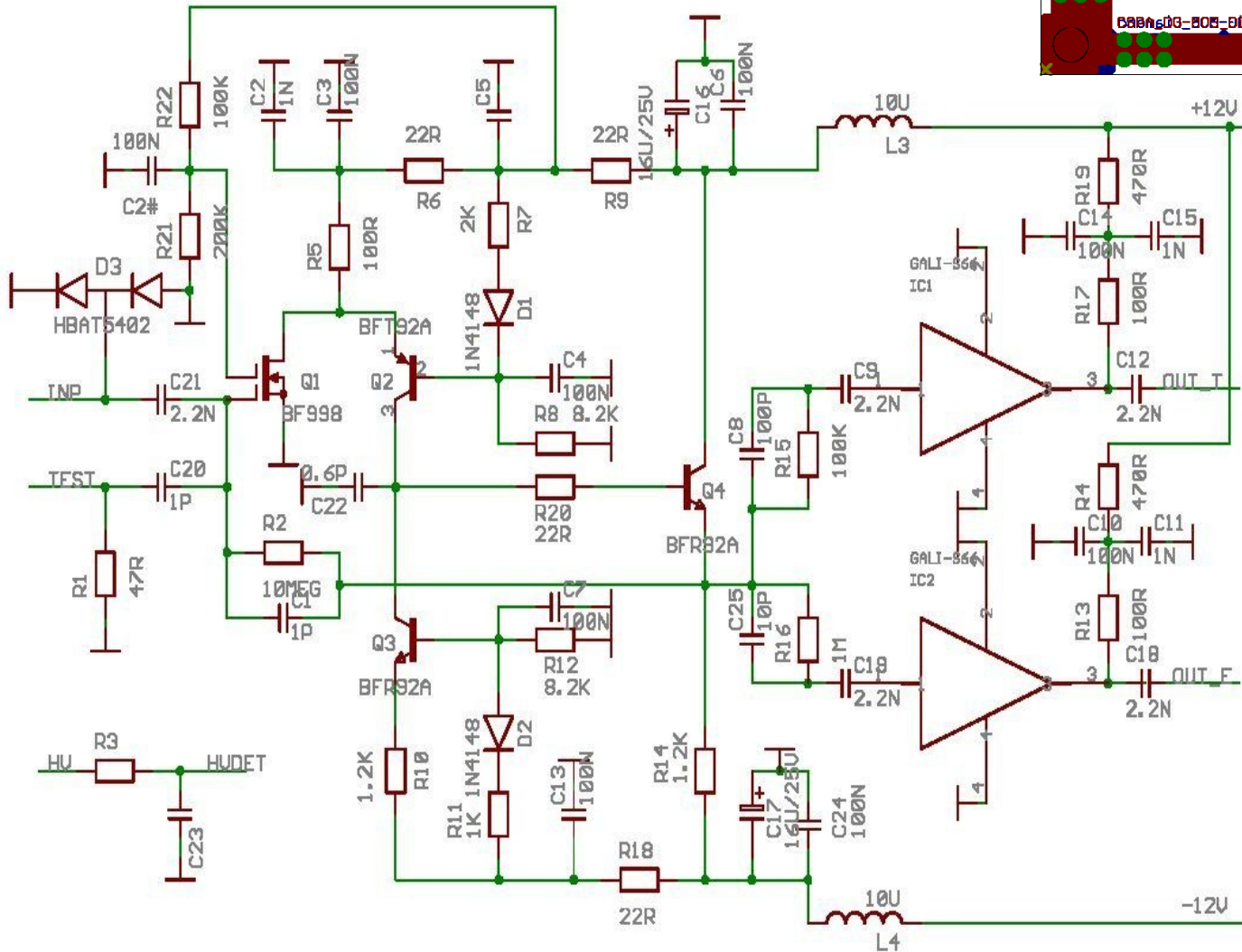
Selected 50% of pulse amplitude

AVERAGE

Selected 1000 samples

Measurements

CSPA – circuit diagram



CS stage

- BF908, DG-MOS
- $C_F = 1\text{pF}$
($S = 1\text{mV/fC}$)
- $\tau_D = 10\mu\text{s}$

Diff+PZC

- $\tau_{\text{diff}} = 5\text{ns}$
- pasive

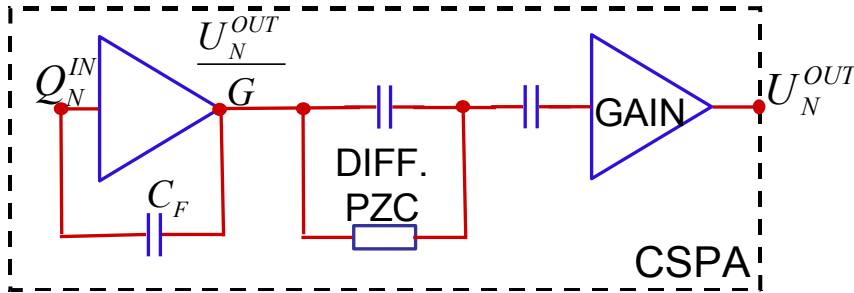
BB stage

- GALI 66, RF block
- Gain ≈ 10

Measurements

CSPA – Noise

► Output noise



► Input noise

$$Q_N^{IN} (e_{RMS}) = \frac{U_N^{OUT} (RMS)}{G} \cdot C_F \cdot \frac{1}{q_e}$$

where: $C_F = 1pF$

$G = 10$

$U_N^{OUT} \approx 1000\mu V_{RMS}$

$q_e = 1.6 \cdot 10^{-19} C$

$$\Rightarrow Q_N^{IN} = 625e_{RMS}$$

(1fC=6250e)

Preamp	Output noise (U_N^{OUT})					Units
No. 1	860	994	970	946	928	μV_{RMS}
No. 2	875	979	994	970	947	μV_{RMS}
Amplit. scale	2	5	10	20	50	$\frac{mV}{div}$

20mV/div
50ns/div
20GS/s

Oscilloscope noise
subtracted

► Comment: S/N ratio for MIPS in SC-DD

W_{DD}	100	200	300	400	500	μm
Q_{MIP}	3k6	7k2	11k8	14k4	18k	e
$\frac{Q_{MIP}}{Q_N}$	5.8	11.5	17.3	23.0	28.8	

Measurements

CSPA – Rise time

► Output signal level $\approx 60\text{mV}$



10mV/div
1ns/div
20GS/s

Generator+osc. rise time
subtracted

► Output signal level $\approx 200\text{mV}$



50mV/div
1ns/div
20GS/s

Generator+osc. rise time
subtracted

► Comment:

$T_R \approx 700\text{ps}$ $B \approx 500\text{MHz}$

$T_w \approx 1\text{ns}/100\mu\text{m}$

(transit. time in SC-DD)



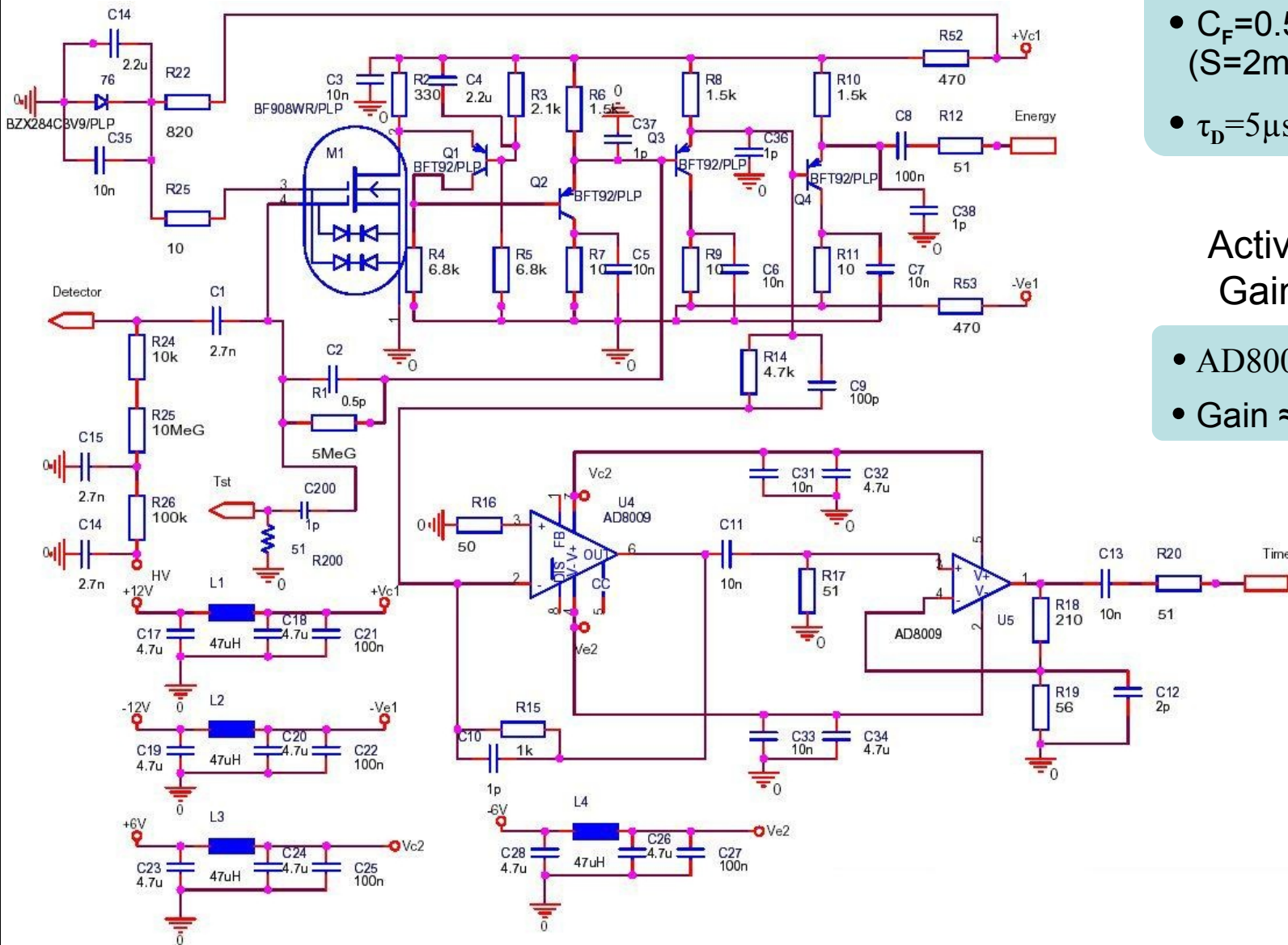
Preamp.	Input transition		Units
	neg.	pos.	
No. 1	753	719	ps
No. 2	666	619	ps

Preamp.	Input transition		Units
	neg.	pos.	
No. 1	775	670	ps
No. 2	688	570	ps

CSPA is fast enough to handle signals
from SC-DD having $W > 100\mu\text{m}$

Measurements

FCSA – circuit diagram



CS stage

- BF908, DG-MOS
- $C_F = 0.5\text{pF}$
($S = 2\text{mV/fC}$)
- $\tau_D = 5\mu\text{s}$

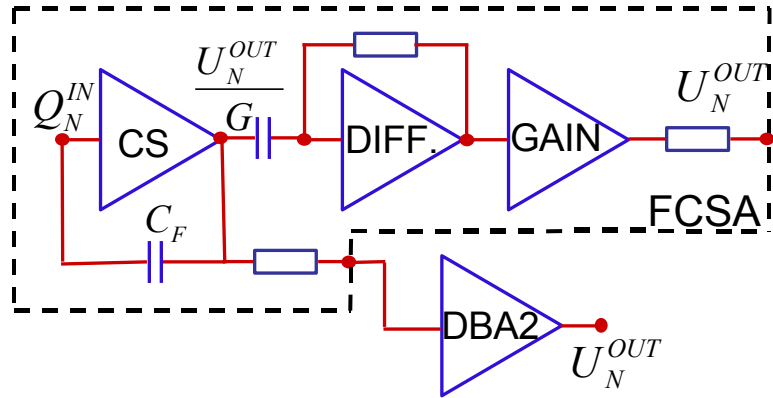
Active Diff.+ Gain stage

- AD8009, CF opamp
- Gain ≈ 80

Measurements

FCSA – Noise

► Output noise



► Input noise

$$Q_N^{IN} (e_{RMS}) = \frac{U_N^{OUT} (RMS)}{G} \cdot C_F \cdot \frac{1}{q_e}$$

where: $C_F = 0.5 \text{ pF}$

$G = 70$ for DBA2

$G = 80$ for Diff.+GAIN

$U_N^{OUT} = \text{see table}$

$q_e = 1.6 \cdot 10^{-19} \text{ C}$

Preamp	Output noise (U_N^{OUT})		Units
	CS+DBA2	CS+Diff.+GAIN	
No. 1	11.08	10.64	mV_{RMS}
No. 2	11.20	10.82	mV_{RMS}

20mV/div
50ns/div
20GS/s

Oscilloscope noise
subtracted

Preamp	Input noise (Q_N^{IN})		Units
	CS	CS+Diff.+GAIN	
No. 1	494	415	e_{RMS}
No. 2	500	423	e_{RMS}

Measurements

FCSA – Rise time

► Output signal level $\approx 120\text{mV}$



$T_R = 2.25\text{ns}$ $B = 155\text{MHz}$
at CS+Diff.+Gain output for
both no.1 and no.2 preamps

20mV/div
2ns/div
20GS/s

Generator+osc.
rise time subtracted

► Comment: time resolution (σ_T) comparison between CSPA and FCSA

$$\sigma_T = \frac{\sigma_N}{\left. \frac{\Delta V}{\Delta T} \right|_{Thr}} \approx \frac{\sigma_N}{U} = \frac{\sigma_N \cdot T_R}{U}$$

CSPA: $\sigma_N = 625 e_{RMS}$

$T_R = 0.7\text{ns}$

$B = 500\text{MHz}$

FCSA: $\sigma_N = 400 e_{RMS}$

$T_R = 2.25\text{ns}$

$B = 155\text{MHz}$

$$\frac{\sigma_T(CSPA)}{\sigma_T(FCSA)} = \frac{\sigma_N(CSPA)}{\sigma_N(FCSA)} \cdot \frac{T_R(CSPA)}{T_R(FCSA)}$$

for the same U



$$\frac{\sigma_T(CSPA)}{\sigma_T(FCSA)} \approx \frac{1}{2}$$

This result was confirmed by beam tests.

Measurements

DBA2 – Noise

Preamp	Input noise					Units
No. 77	13.9	21.0	24.1	23.2	22.7	μV_{RMS}
No. 16	13.9	20.7	23.7	22.8	22.3	μV_{RMS}
Amplit. scale	2	5	10	20	50	$\frac{\text{mV}}{\text{div}}$

50ns/div
20GS/s

Oscilloscope noise subtracted

DBA2 – Rise time

Preamp.	No. 77	No. 16	Units
T_R	160	135	ps
B	2.2	2.6	GHz
G	140	134	

500ps/div
50mV/div
20GS/s

Gen.+osc.
rise time
subtracted

Output signal level \approx 200mV

BB4 – Noise

Channel	1	2	3	4	Units
Input noise	14.5	13.8	14.2	14.3	μV_{RMS}

50ns/div
20mV/div
20GS/s

Oscilloscope noise subtracted

BB4 – Rise time

Channel	1	2	3	4	Units
T_R	314	328	320	320	ps
B	≈ 1.1				GHz
G	201	204	211	204	

Counting rate effects

Baseline shift

- ▶ Campbell theorem (of mean square)

Randomly appearing pulses

Average rate n

Pulse shape $u(t)$



$$\overline{u^2} = n \int_{-\infty}^{+\infty} |u(t)|^2 dt$$

baseline shift

- ▶ Case of exponential shape

$$u(t) = A \cdot e^{-\frac{t}{\tau}}$$



$$\sqrt{\overline{u^2}} = 0.7 \cdot A \sqrt{n\tau}$$

- ▶ Examples

Charge sens.
amps.

MIP particles
SC-DD, 350 μ
CSA, $C_F=1$ pF

$A=2$ mV
 $\tau=10$ μ s
 $n=10^9$ p/s

shift = 140mV

Shaping
amps.

$G=200$
 $\tau=10$ ns

$A=400$ mV
 $\tau=10$ ns
 $n=10^9$ p/s

shift = 885mV

Counting rate effects

Amplitude distortion

► Defining the problem

Randomly appearing pulses

Linear range U_L

Pulse shape $u(t) = A \cdot e^{-\frac{t}{\tau}}$



$n(1\%) = ?$

(counting rate corresponding to 1% distorted pulses in nonlinear region)

► Solution (derived from Campbell's theorem)

CSamp, AC coupled

$$n_{AC} = \frac{1}{3.12\tau} \left[\frac{U_L - A}{A} \right]^2$$

$$n_{AC} \approx \frac{1}{3.12\tau} \left[\frac{U_L}{A} \right]^2 \text{ if } \frac{U_L}{A} \geq 20$$

CSamp, DC coupled

$$n_{DC} \approx \frac{1}{\tau} \left[\frac{U_L}{A} \right]$$

$$\text{if } \frac{U_L}{A} \geq 20$$

Ratio

$$\frac{n_{AC}}{n_{DC}} = \frac{1}{3.12} \cdot \frac{U_L}{A}$$

► Examples

n_{AC}

$\frac{U_{lin}}{A} \backslash \tau$	0.5	1	10 (μs)
20	$2.6 \cdot 10^8$	$1.3 \cdot 10^8$	$1.3 \cdot 10^7$
100	$6.4 \cdot 10^9$	$3.2 \cdot 10^9$	$3.2 \cdot 10^8$
1000	$6.4 \cdot 10^{11}$	$3.2 \cdot 10^{11}$	$3.2 \cdot 10^{10}$

n_{DC}

$\frac{U_{lin}}{A} \backslash \tau$	0.5	1	10 (μs)
20	$4 \cdot 10^7$	$2 \cdot 10^7$	$2 \cdot 10^6$
100	$2 \cdot 10^8$	$1 \cdot 10^8$	$1 \cdot 10^7$
1000	$2 \cdot 10^9$	$1 \cdot 10^9$	$1 \cdot 10^8$

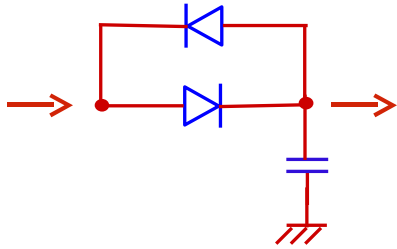
Ideas for future development

- ▶ The purpose: to improve time resolution $\sigma_T = \frac{\sigma_N}{slope}$
- ▶ Present status:
 - BB amps are too noisy
 - CS amps have too slow slope (imposed by transit time in SC-DD)
- ▶ Ideas for improvements:
 - Linear filter reduces the noise but in the same time worsens signals rise time (slope). Nonlinear filter which acts different on noise (low amplitude) and on signal (larger amplitude) may be a good idea.
 - A thinner SC-DD has a shorter transit time and to compensate for smaller charge, it is possible to put in parallel a few thin crystals.

Ideas for future development

Nonlinear filter

❖ idea...



integrator

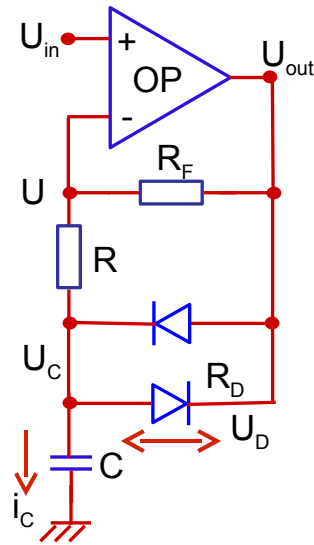
$$T_{int} = C \cdot R_D(U_D)$$

$R_D = \text{high}$ (noise)

$R_D = \text{low}$ (signal)

the simplest nonlinear integrator

❖ this really works...



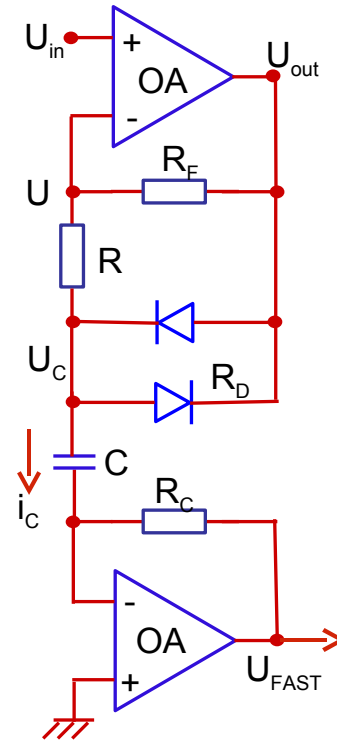
...because we can control diodes opening

$$U_D = [U_{in} - U_C] \cdot \left[1 + \frac{R_F}{R} \right]$$

Attention!

$$i_C = C \cdot \frac{dU_C}{dt} \quad \text{Faster signal than } U_C!$$

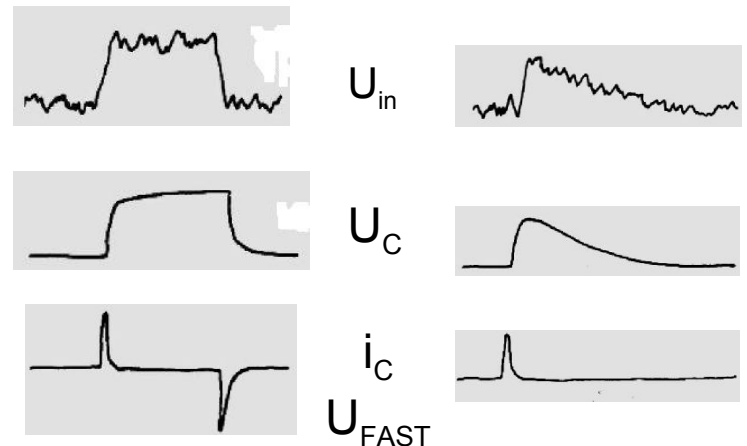
❖ this works better...



because it takes the advantage of using fast signal i_C converted in U_{FAST}

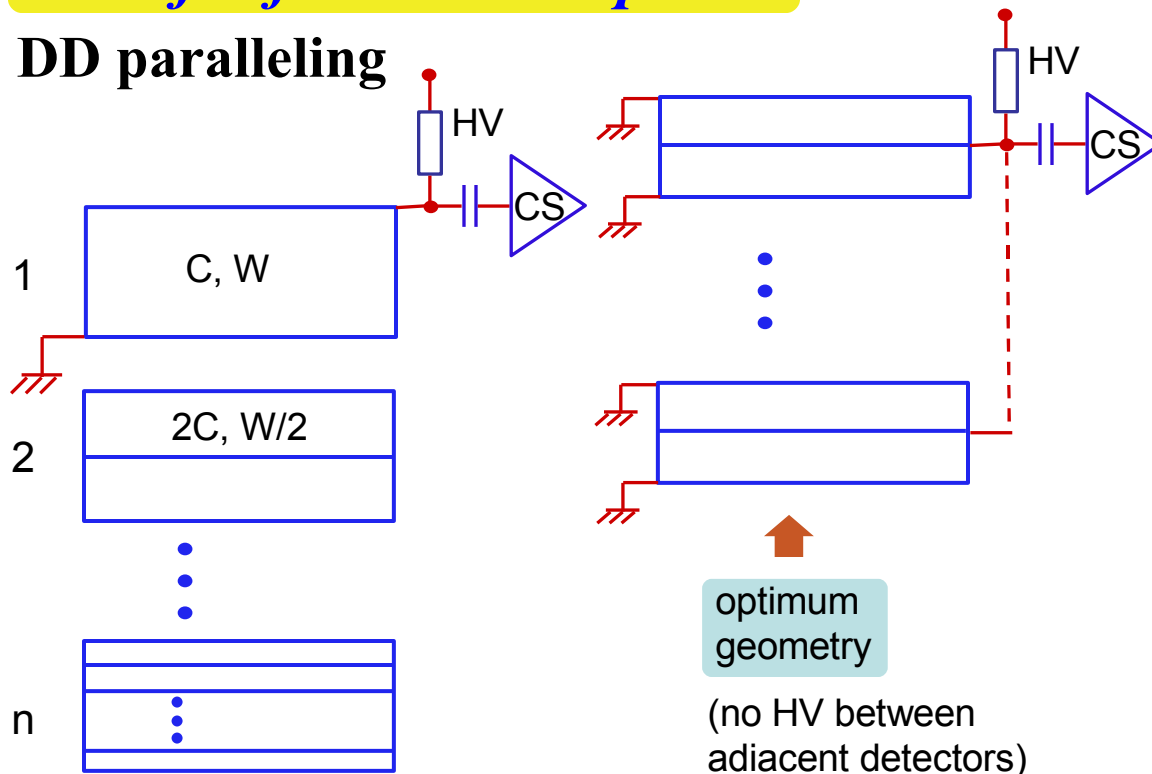
$$U_{FAST} = R_C \cdot i_C = R_C C \cdot \frac{dU_C}{dt}$$

❖ signal and noise handling...



Ideas for future development

DD paralleling



► Example:

n	1	4
W	400 μ	100 μ
ϕ_{cont}	2mm	2mm
S_{cont}	3mm ²	3mm ²
C	0.37pF	6pF
T_w	4ns	1ns

* the same charge collected

No. of DD	1	2	n
Width	W	$\frac{W}{2}$	$\frac{W}{n}$
Cap. (total)	C	4C	n^2C
Transit. time	T_w	$\frac{T_w}{2}$	$\frac{T_w}{n}$

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